

Report in Accordance with BFRC Guidelines and Regulations

Product description: Made For Trade Korniche Bi-Fold Doorset

CONFIDENTIAL

Client:	Aanco (UK) Ltd T/A Made For Trade Wellington House, Wynyard Avenue Wynyard Billingham TS22 5TB
Project:	Aluminium Korniche Bi-Fold Doorset
Project reference:	CU21577-34
Prepared By:	Richard Bate Technical Director
Issue date:	16 May 2022

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Approved Simulator 001

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1 Introduction

The U-value calculations of the Made For Trade, Korniche bi-fold doorset detailed below were commissioned by Ashley Gaunt of Made For Trade.

2 Validation of Program

The BISCO 12.0 analysis software has been validated against proofs in Annex I (I1 to I10) of BS EN ISO 10077-2:2017.

3 Analysis Method

The frame profile results detailed below are provided by computer simulation using BISCO 12.0 software program and BFRC guidelines and regulations.

4 Summary of Results

A summary of results are detailed in the following sections. The details supplied for the analysis as well as all information required to verify the analysis can be found in the attached CD.

4.1 Frame thermal transmittance (following the principles of BS EN ISO 10077-2)

Frame Profile	Frame Thermal Transmittance (U_f)
Head	3.2 W/(m ² ·K)
Left Jamb	3.0 W/(m ² ·K)
Right Jamb	3.2 W/(m ² ·K)
Threshold	3.2 W/(m ² ·K)
Meeting Stile	2.9 W/(m ² ·K)

4.2 Linear thermal transmittance (following the principles of BS EN ISO 10077-2)

Frame Profile	Linear Thermal Transmittance (ψ)
Head	0.024 W/(m·K)
Left Jamb	0.029 W/(m·K)
Right Jamb	0.024 W/(m·K)
Threshold	0.024 W/(m·K)
Meeting Stile	0.051 W/(m·K)

4.3 Centre pane U-Value of glazing calculated in accordance with BS EN 673.

Glazing Unit	Centre Pane U-value (U_g)
4-18-6.8 Low-E 0.05 uncorrected emissivity (St Gobain Planitherm Total+), 90% Argon 10% Air filled, float outer pane (St Gobain Planiclear) glazing unit with Superspacer Premium spacer bar with 5mm hot melt butyl secondary seal.	1.2 W/(m ² ·K)

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4.4 The thermal performance of the doorsets (U_D) in accordance with BFRC guidelines and regulations:

Korniche Frame Profile	Doorset U-Value
Aluminium frame system with 4-18-6.8 Low-E 0.05 uncorrected emissivity (St Gobain Planitherm Total+), 90% Argon 10% Air filled, float outer pane (St Gobain Planiclear) glazing unit with Superspacer Premium spacer bar with 5mm hot melt butyl secondary seal.	1.8 W/(m ² ·K)

4.6 The Effective L_{50} in accordance with BFRC guidelines and regulations:

Frame Profile	Effective L_{50}
Air permeability at 50 pa	0.00 W/(m ² ·K)

4.7 Total solar energy transmittance (g) in accordance with EN 410

Korniche Frame Profile	$g_{doorset}$
Aluminium frame system with 4-18-6.8 Low-E 0.05 uncorrected emissivity (St Gobain Planitherm Total+), 90% Argon 10% Air filled, float outer pane (St Gobain Planiclear) glazing unit with Superspacer Premium spacer bar with 5mm hot melt butyl secondary seal.	0.47


5.0 BFRC Rating

5.1 Made For Trade Korniche Bi-Fold doorset system

Korniche Frame Profile	Rating
Aluminium frame system with 4-18-6.8 Low-E 0.05 uncorrected emissivity (St Gobain Planitherm Total+), 90% Argon 10% Air filled, float outer pane (St Gobain Planiclear) glazing unit with Superspacer Premium spacer bar with 5mm hot melt butyl secondary seal.	- 19 (Rating Scale C)

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6.0 Authorisation

	Prepared by:
Signature:	
Name:	Richard Bate
Title:	Technical Director

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Technical Specification

Profiles	Ref. No.	Material Type/Manufacturer's Name & Density (Timber only)	Dimensions (Height & Width)
Head	A-04105	Made For Trade, thermally broken aluminium	Outer frame - 56mm x 84mm Sash – 60mm x 75mm
Left Jamb	A-04104	Made For Trade, thermally broken aluminium	Outer frame - 56mm x 84mm Sash – 82mm x 83mm
Right Jamb	A-04103	Made For Trade, thermally broken aluminium	Outer frame - 56mm x 84mm Sash – 60mm x 75mm
Threshold	A-04114	Made For Trade, thermally broken aluminium	Outer frame - 56mm x 84mm Sash – 60mm x 75mm
Meeting Stile	A-04117	Made For Trade, thermally broken aluminium	60mm x 75mm

Glazing Component	Specification
Overall sealed unit: 1. Thickness (mm)	1. 28.8mm
Outer pane 1. Thickness (mm) 2. Manufacturer 3. Description	1. 4mm 2. St Gobain 3. Planiclear
Inner pane: 1. Thickness 2. Manufacturer 3. Description	1. 6.8mm 2. St Gobain 3. Laminated Planitherm Total+
Spacer bar: 1. Manufacturer 2. Description	1. Edgetech 2. Superspacer Premium
Cavity 1. Distance (mm) 2. Gas %	1. 18mm 2. Argon 90% Air 10%
Edge seal 1. Manufacturer 2. Description	1. N/A 2. 5mm hot melt butyl secondary seal

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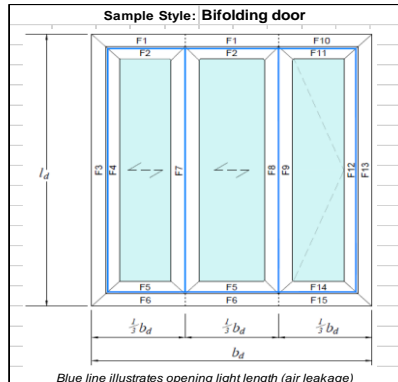
Additional Notes

Air leakage data is taken from Build Check Test report ref. W22208-1 dated May 2022 (data at 50Pa pressure = 0.05).

Solar heat gain figures are calculated from g-values supplied by the product manufacturer from EN 410 calculations for the glass units used in this simulation. The value used is 0.72.

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BFRC Spreadsheet



Report Number: U21577-34 Issue 2.3: 04/01/2016
 Report Date: 22 April 2022
 Project Details: Aluminium Bi-fold Doorset

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Input Values:
 Yellow input, green intermediary, blue final X DP is no. of decimal places to enter

Parameter	Symbol	Units
Total door height ODP	l_d	2180 mm
Total door width ODP	b_d	2500 mm

Frame offset: **No**

Nominal 4mm etc to **ODP**, others **1DP**

Glazing dimensions and properties:

Thickness of pane 1	4	mm
Pane 1/2 distance	18	mm
Gas fill (1/2)	Argon 90%	
Thickness of pane 2	6.8	mm
Complete next 3 cells for TG IGU		
Pane 2/3 distance		mm
Gas fill (2/3)		
Thickness of pane 3		mm
Glazing Trans. - 3DP	U_g	1.204 W/(m²·K)
g-value - 2DP	g	0.72

Thermal transmittance of door from hot box test

$U_d - 2DP$ W/(m²·K)

Frame dimensions: All frame values to nearest mm, gaskets to nearest 0.1mm

Section	Frame height, b_f (mm)	Gasket protrusion, b_g (mm)	Frame with gasket (mm)	Total frame (mm)
F1 + F2 L&M head rail	F1 left fixed head	56	n/a	56.0
	F2 left opening head	50	0.0	50.0
F3 + F4 left jamb	F3 left fixed jamb	56	n/a	56.0
	F4 left opening jamb	54	0.0	54.0
F5 + F6 L&M threshold	F5 left opening threshold	50	0.0	50.0
	F6 left fixed threshold	56	n/a	56.0
F7 Meeting Stile	F7 Meeting Stile	132	0.0	132.0
	F8 bi-fold opener	60	0.0	60.0
F8 + F9 Meeting stile	F9 opener	72	0.0	72.0
	F10 right fixed head	56	n/a	56.0
F10 + F11 right head rail	F11 right opening head	50	0.0	50.0
	F12 right opening jamb	50	0.0	50.0
F12 + F13 right jamb	F13 right fixed jamb	56	n/a	56.0
	F14 right opening threshold	50	0.0	50.0
F14 + F15 R threshold	F15 right fixed threshold	56	n/a	56.0
	Recession depth F6 & F15:			
Total gasket area				0 m²

Door Dimensions:

Section	Length		Width		Area	
	(m)	(m)	(m)	(m)	No gasket (for U-value) (m²)	With gasket (for g-value) (m²)
Left Sliding light	1.9680	0.6573	1.2936	1.2936		
Middle Sliding light	1.9680	0.7073	1.3920	1.3920		
Right Opening light	1.9680	0.6553	1.2897	1.2897		
Total glazing, A_g					3.9754	3.9754
Frame	(m)	(m)	(m²)	(m²)		
F1	1.6667	0.0560	0.0918	0.0918		
F2	1.6107	0.0500	0.0744	0.0744		
F3	2.1800	0.0560	0.1189	0.1189		
F4	2.0680	0.0540	0.1090	0.1090		
F5	1.6107	0.0500	0.0744	0.0744		
F6	1.6667	0.0560	0.0918	0.0918		
F7	2.0680	0.1320	0.2664	0.2664		
F8	2.0680	0.0600	0.1211	0.1211		
F9	2.0680	0.0720	0.1453	0.1453		
F10	0.8333	0.0560	0.0451	0.0451		
F11	0.7773	0.0500	0.0358	0.0358		
F12	2.0680	0.0500	0.1009	0.1009		
F13	2.1800	0.0560	0.1189	0.1189		
F14	0.7773	0.0500	0.0358	0.0358		
F15	0.8333	0.0560	0.0451	0.0451		
Total Frame					1.4746	1.4746
Total door, A_d					5.4500	5.4500
Percentage left light glass area					23.74%	23.74%
Percentage middle light glass area					25.54%	25.54%
Percentage right light glass area					23.66%	23.66%
Percentage glass area (total)					72.94%	72.94%

Where a U_d value from hot box testing is available, no $L_{f,2D}$ or $L_{\psi,2D}$ values need to be entered

Frame conduction: All L values to **4DP**. All b values to **ODP**

Section	All L values to 4DP		All b values to ODP	
	$W/(m^2 \cdot K)$	b_p (mm)	$W/(m^2 \cdot K)$	b_g (mm)
F1 + F2 L&M head rail	0.5330	190	0.5940	190
F3 + F4 left jamb	0.5240	190	0.5900	190
F5 + F6 L&M threshold	0.5320	190	0.5930	190
F7 Meeting Stile	0.7600	380	0.8860	380
F8 + F9 Meeting stile	0.7600	380	0.8860	380
F10 + F11 right head rail	0.5330	190	0.5940	190
F12 + F13 right jamb	0.5300	190	0.5910	190
F14 + F15 R threshold	0.5320	190	0.5930	190

Frame:

Section	Frame widths (no gaskets), B_f (m)	Frame U-value, U_f (W/(m²·K))	Frame areas (no gaskets), A_f (m²)	Frame heat flow, H_U (W/K)	Linear trans, ψ (W/(m·K))	Linear length, l_g (m)	Junction Heat flow, H_{ψ} (W/K)
F1 + F2 L&M head rail	0.1060	3.2230	0.1661	0.5355	0.0236	1.3647	0.0322
F3 + F4 left jamb	0.1100	3.0239	0.2279	0.6892	0.0286	1.9680	0.0563
F5 + F6 L&M threshold	0.1060	3.2135	0.1661	0.5339	0.0236	1.3647	0.0322
F7 Meeting Stile	0.1320	2.8581	0.2664	0.7613	0.0512	1.9680	0.1008
F8 + F9 Meeting stile	0.1320	2.8581	0.2664	0.7613	0.0512	1.9680	0.1008
F10 + F11 right head rail	0.1060	3.2230	0.0809	0.2608	0.0236	0.6553	0.0155
F12 + F13 right jamb	0.1060	3.1947	0.2198	0.7023	0.0236	1.9680	0.0465
F14 + F15 R threshold	0.1060	3.2135	0.0809	0.2600	0.0236	0.6553	0.0155
Totals					1.4746	4.5044	0.3997

Solar Factor, g-value:

F_d	0.9
g_d	0.47

Other parameters:

$\lambda_p = 0.035$ W/(m·K)	$R_{se} = 0.04$ m²·K/W	Panel thickness, $d_p = d_g = 0.0288$ m	$R_{se} = 0.13$ m²·K/W
$R_p = 0.8229$ m²·K/W	$R_{tot} = 0.9929$ m²·K/W	$U_p = 1.0072$ W/(m²·K)	

Air Leakage loss:

Air leakage at 50 Pa per hour & per unit length of opening light (BS 6375-1) - 2DP	0.05 m³/(m·h)
Opening light length L_{50} 13.0480 m	Total air leakage 0.652 m³/h
L_{50} 0.12 m³/(m²·h)	Heat loss = 0.0165 L_{50} 0.00 W/(m²·K)

Energy Window
 Energy Index
-19
 Window Rating
C

BFRC Rating
 kWh/(m²·yr)
 ≥20 **A++**
 >10 to 20 **A+**
 0 to <10 **A**
 <-10 to <-10 **B**
 <-20 to <-10 **C** ✓
 <-30 to <-20 **D**
 <-50 to <-30 **E**

BFRC Rating =
218.6g_{door} - 68.5 x (U_{door} + Effective L₅₀) = -18.61

Climate zone is: **UK**

Thermal transmittance, W/(m²·K) U_{door} **1.8**

Solar factor g_{door} **0.47**

Door air leakage heat loss, W/(m²·K) L_{factor} **0.00**

BFRC Certified Simulator No **001**

Simulator Name: **Richard Bate**

BS EN 673 Spreadsheet

Version 12 18/06/2015. Calculations according to BS EN 673:2011

Number of spaces	Help																			
1																				
Spaces 1																				
Glazing orientation	Vertical																			
Resistivity panes	1	m·K/W																		
Outside																				
<table border="1" style="margin: auto;"> <tr> <td style="writing-mode: vertical-rl; transform: rotate(180deg);">P a n e 1</td> <td style="text-align: center;">90%</td> <td style="writing-mode: vertical-rl; transform: rotate(180deg);">P a n e 2</td> </tr> </table>			P a n e 1	90%	P a n e 2															
P a n e 1	90%	P a n e 2																		
<table border="1" style="margin: auto;"> <tr> <td>Calculate</td> <td colspan="2">Gas</td> </tr> <tr> <td></td> <td colspan="2">Argon</td> </tr> <tr> <td>Thickness (mm)</td> <td>4.0</td> <td>18</td> <td>6.8</td> </tr> <tr> <td>Normal emissivity</td> <td>0.89</td> <td>0.05</td> <td style="background-color: red;"></td> </tr> <tr> <td>$\sum d_i r_i =$</td> <td colspan="3">0.0108</td> </tr> </table>			Calculate	Gas			Argon		Thickness (mm)	4.0	18	6.8	Normal emissivity	0.89	0.05		$\sum d_i r_i =$	0.0108		
Calculate	Gas																			
	Argon																			
Thickness (mm)	4.0	18	6.8																	
Normal emissivity	0.89	0.05																		
$\sum d_i r_i =$	0.0108																			
Uncoated																				

For uncoated surfaces input 0.89 for normal emissivity, which corresponds to a corrected emissivity of 0.837

External, R_{se}	0.04	$(m^2 \cdot K)/W$
Internal, R_{si}	0.13	$(m^2 \cdot K)/W$
Iteration number	U value	$\sum 1/h_s$
	$W/(m^2 \cdot K)$	$(m^2 \cdot K)/W$
1	1.204	0.65
2	1.204	0.65

λ_{eff}	ΔT
$W/(mK)$	
0.0277	15
0.0277	15

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Spacer Conductivity

May 2014 – No. W21 – Revision Index 3.06/2021 – valid until June 30th, 2023

'WARM EDGE' WORKING PARTY



Data sheet Psi values for windows

Only valid for use with hot-melt-sealant

based on determination of the equivalent thermal conductivity of spacers by measurement



Edgetech Europe GmbH
Gladbacher Straße 23
D-52525 Heinsberg

Profile description	Super Spacer Premium		Spacer height in mm	Material	Thickness d in mm
			4.7		
			Spacer category E	Mylar foil Silicone foam	0.10 4.7

Representative frame profiles	Representative glass constructions	Metal with thermal break	Plastic	Wood	Wood/Metal
Representative psi value double-glazed thermally insulated glass in W/m ² K	 Double-sheet insulating glass $U_g=1.1$ W/m ² K	0.035	0.031	0.030	0.031
Representative psi value triple-glazed thermally insulated glass in W/m ² K	 Triple-sheet insulating glass $U_g=0.7$ W/m ² K	0.030	0.029	0.028	0.029

Two Box model Characteristic values		Space between panes in mm	$\lambda_{eq,2b}$ in W/mK	
		Can be used for all spacer widths	Box 1 - $h_1 = 5$ mm	Box 2 - $h_2 = 4.7$ mm
			0.24	0.15

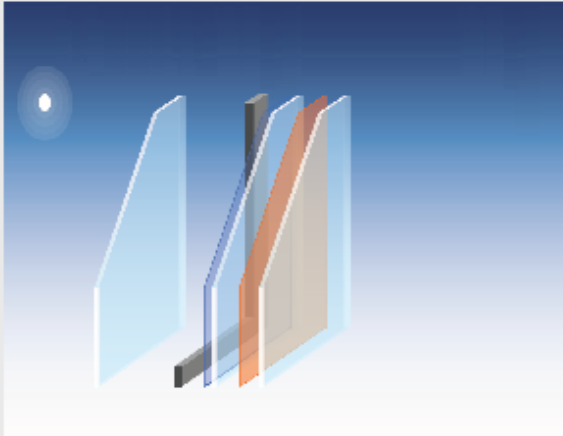
Explanation
The equivalent thermal conductivity has been determined in accordance with the ift guideline WA-17engl/1 "Thermally improved spacers – Determination of the equivalent thermal conductivity by measurement". The representative linear heat transfer coefficients calculated in this way (representative psi values) apply to typical frame profiles and glazing for the determination of the heat transfer coefficient U_w of windows. They have been determined under the boundary conditions (frame profiles, glazing, glass mounting depth, back covering, primary and secondary sealant) defined in the ift guideline WA-08engl/3 "Thermally improved spacers – Part 1: Determination of the representative Psi value for window frame profiles". This guideline also governs the area of validity and application of the representative psi values. In order to avoid rounding errors, the psi values in the data sheet have been given at 0.001 W/mK. The method for the arithmetical determination of the psi values has an accuracy of ± 0.003 W/mK. Differences of less than 0.005 W/mK are not significant. For further information, refer to the Bulletin 004/2008 "Guide to Warm Edge" of Bundesverband Flachglas.

Characteristic values determined by:



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G-Value Source



Glazing 1	PLANICLEAR 4 mm
Cavity 1	Argon 90% 18 mm
Glazing 2	PLANITHERM TOTAL+ FG PLANICLEAR 3 mm PVB STANDARD 0.76 mm PLANICLEAR 3 mm

Last name: Sue Peatey
Country: United Kingdom

Notes:

<p>LUMINOUS FACTORS EN410 (2011-04)</p> <p>Light Transmittance (TL) 79 % Outdoor Reflectance (RLe) 13 % Indoor Reflectance (RLI) 12 %</p> <p>THERMAL TRANSMISSION EN673-2011</p> <p>Ug 1.2 W/(m².K) Angle relative to the vertical 0 °</p> <p>MANUFACTURING SIZES</p> <p>Nominal Thickness 28.76 mm Weight 25.8 kg/m²</p> <p>ACOUSTICS EN 12758</p> <p>Rw (C;Ctr) N/A STC (ASTM E413) N/A OITC (ASTM E1332) N/A</p> <p>SAFETY CLASS EN 12800</p> <p>Pendulum Body Resistance NPD/1B1</p>	<p>ENERGY FACTORS EN410 (2011-04)</p> <p>Transmittance (TE) 59 % Outdoor Reflectance (Ree) 20 % Indoor Reflectance (Rel) 17 % Absorptance A1 (AE1) 6 % Absorptance A2 (AE2) 15 %</p> <p>SOLAR FACTORS EN410 (2011-04)</p> <p>Solar Factor (g) 0.72 Shading Coefficient (SC) 0.83</p> <p>COLOR RENDERING</p> <p>Transmission (Ra) 99 Reflection (Ra) 90</p> <p>ANTI-BURGLARY EN 358</p> <p>Burglar Resistance NPD/P1A</p> <p>CARBON FOOTPRINT EN 15804+A2</p> <p>Global Warming Potential (GWP) (kg, CO₂ equiv/m²) European average 47.58</p>
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Calumen calculates the photometric characteristics and thermal transmission of glass using calculation algorithms which comply with the following standards: the European standards EN 410 and EN 673, the international standard ISO9050, the Japanese standard JIS R 3106/3107 and the Korean standard KS L 2514/2525. The functional output and calculation rules of Calumen for standards EN 410 and EN 673 have been validated by TÜV Rheinland (report 11923R-11-33705). The technical performances obtained according to these standards are provided for information only and are subject to amendment. Only the values entered in the performance declaration available on the CE marking site of Saint-Gobain Glass are official. The sound attenuation indices are measured under laboratory conditions according to the standards EN ISO 10140 and EN 12758. The calculated indices are provided for information only. The accuracy for Rw index lies within a range of +/-2dB. The glass thickness calculations comply with the 2012 version of the DTU39-P4 description. The USER is responsible for ensuring that the correct calculation hypotheses are entered and the DTU39 is applied appropriately for the project concerned.

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Air Leakage Test Evidence



Glazing Component	Specification
Overall sealed unit: 1. Thickness (mm)	1. 28mm
1. Outer pane 2. Cavity 3. Inner pane	1. 4mm clear toughened glass 2. 20mm 3. 4mm clear toughened glass

The above specimen description has been supplied by the client and not verified by Build Check.

Dimensions: Outer frame (w x h): 2500mm x 2180mm

3. Test Details

Test Date: 14 April 2022

Test performed by: Angelo Wells

Test carried out at Build Check Ltd's test laboratory, Unit 3 Lincoln Park Business Centre, Lincoln Road, High Wycombe, HP12 3RD

Test conditions in accordance with standard.

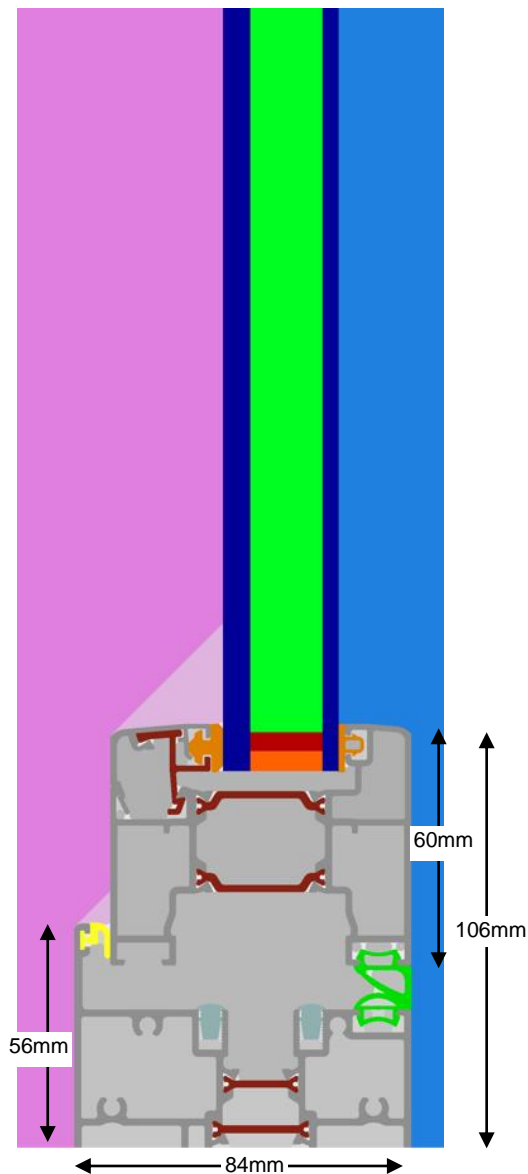
4. Results

Air Pressure (Pa)	Average between positive and negative pressure				Mean	
	Positive pressure		Negative pressure		Per m ² area (m ³ /h-m)	Per m opening length (m ³ /h-m)
	Net permeability per m ² area (m ³ /h-m ²)	Net permeability per m opening length (m ³ /h-m)	Net permeability per m ² area (m ³ /h-m ²)	Net permeability per m opening length (m ³ /h-m)		
50	0.15	0.06	0.10	0.04	0.13	0.05

* During the test, the chamber leakage was greater than 30% of the combined chamber and specimen leakage rate.

Appendix - Profile Drawings

Head



BISCO Calculation Results

BISCO data file: A-04105 head.bsc

Number of nodes = 69031

Heat flow divergence for total object = 0.000746013

Heat flow divergence for worst node = 0.913472

Thermal transmittance of frame (EN 10077-2)

$U_f = (Q / (t_i - t_e) - U_{p1} * w_{p1} - U_{p2} * w_{p2}) / w_f = -3.427 \text{ W}/(\text{m}^2 \cdot \text{K})$

Thermal coupling coefficient

$L2D = Q / (t_i - t_e) = 0.594 \text{ W}/(\text{m} \cdot \text{K})$

$Q = 11.876 \text{ W}/\text{m}$

$t_i = 20.00^\circ\text{C}$

$t_e = 0.00^\circ\text{C}$

$U_{p1} = 5.033 \text{ W}/(\text{m}^2 \cdot \text{K})$ (top edge of bitmap)

$w_{p1} = 0.1900 \text{ m}$ (distance no. 2)

$U_{p2} = 0.000 \text{ W}/(\text{m}^2 \cdot \text{K})$

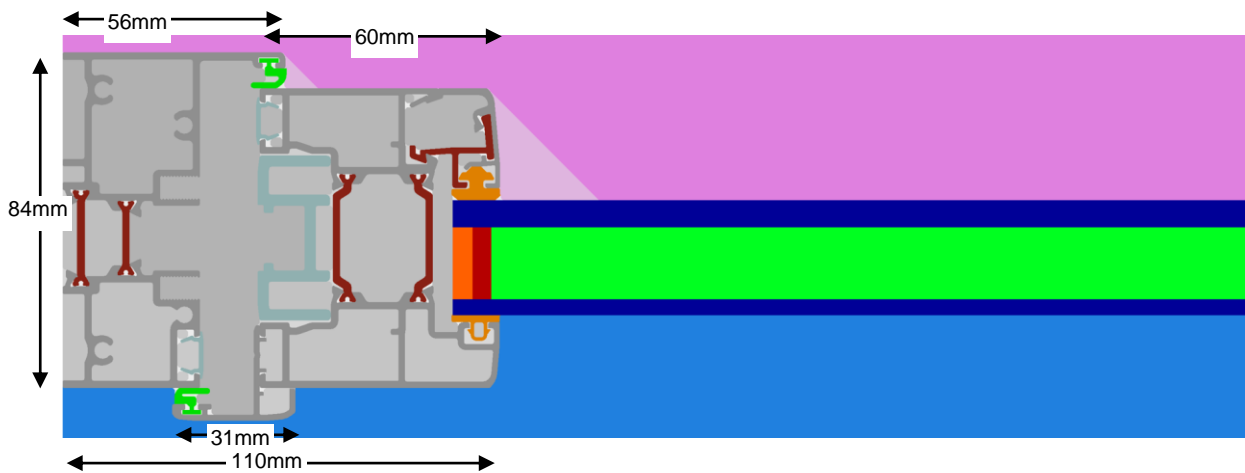
$w_{p2} = 0.0000 \text{ m}$

$w_f = 0.1058 \text{ m}$ (distance no. 1)

	Material	Thermal Conductivity W/(m.K)
	PVC-U Rigid, BS EN 10077-2	0.17
	PVC Flexible, BS EN 10077-2	0.14
	Aluminium, BS EN 10077-2	160.0
	Soda Lime Glass, BS EN 10077-2	1.0
	Superspacer Premium, IFT Rosenheim report 13-002649-PR02 (declared value)	0.15
	Hot Melt Butyl, BS EN 10077-2	0.24
	Polyurethane Foam, BS 10456	0.05
	EPDM, BS EN 10077-2	0.25
	Polyamide, BS EN 10077-2	0.30

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Left Jamb



BISCO Calculation Results

BISCO data file: A-04104 left jamb.bsc

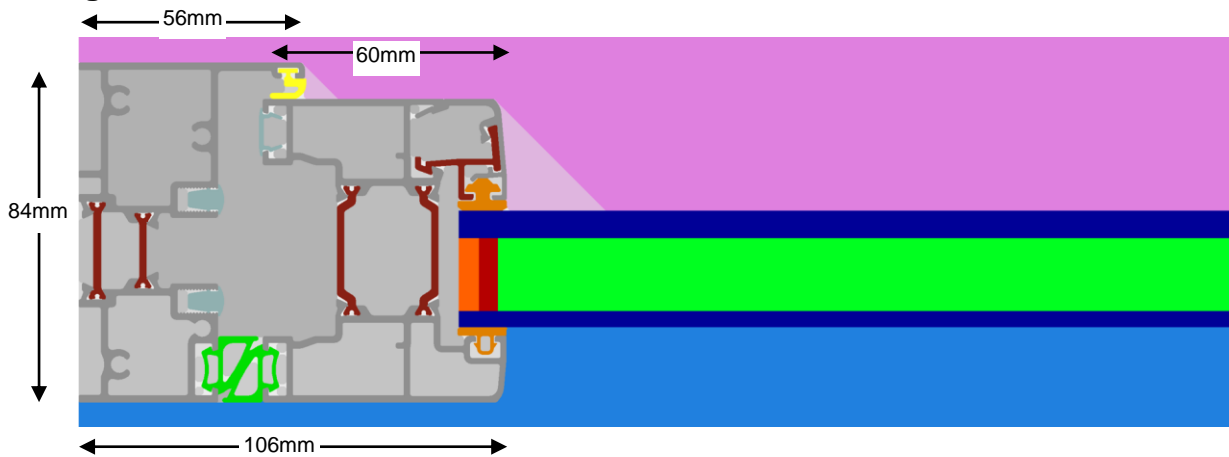
Number of nodes = 72083
 Heat flow divergence for total object = 2.81387e-05
 Heat flow divergence for worst node = 0.459044

Thermal transmittance of frame (EN 10077-2)
 $U_f = (Q / (t_i - t_e) - U_{p1} * w_{p1} - U_{p2} * w_{p2}) / w_f = -3.335 \text{ W}/(\text{m}^2 \cdot \text{K})$
 Thermal coupling coefficient
 $L2D = Q / (t_i - t_e) = 0.590 \text{ W}/(\text{m} \cdot \text{K})$
 $Q = 11.798 \text{ W}/\text{m}$
 $t_i = 20.00^\circ\text{C}$
 $t_e = 0.00^\circ\text{C}$
 $U_{p1} = 5.033 \text{ W}/(\text{m}^2 \cdot \text{K})$ (right edge of bitmap)
 $w_{p1} = 0.1900 \text{ m}$ (distance no. 2)
 $U_{p2} = 0.000 \text{ W}/(\text{m}^2 \cdot \text{K})$
 $w_{p2} = 0.0000 \text{ m}$
 $w_f = 0.1099 \text{ m}$ (distance no. 1)

	Material	Thermal Conductivity W/(m.K)
	PVC-U Rigid, BS EN 10077-2	0.17
	PVC Flexible, BS EN 10077-2	0.14
	Aluminium, BS EN 10077-2	160.0
	Soda Lime Glass, BS EN 10077-2	1.0
	Superspacer Premium, IFT Rosenheim report 13-002649-PR02 (declared value)	0.15
	Hot Melt Butyl, BS EN 10077-2	0.24
	Polyurethane Foam, BS 10456	0.05
	EPDM, BS EN 10077-2	0.25
	Polyamide, BS EN 10077-2	0.30

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Right Jamb



BISCO Calculation Results

BISCO data file: A-04103 right jamb.bsc

Number of nodes = 69251

Heat flow divergence for total object = 0.000803807

Heat flow divergence for worst node = 0.607267

Thermal transmittance of frame (EN 10077-2)

$U_f = (Q / (t_i - t_e) - U_{p1} * w_{p1} - U_{p2} * w_{p2}) / w_f = -3.453 \text{ W}/(\text{m}^2 \cdot \text{K})$

Thermal coupling coefficient

$L2D = Q / (t_i - t_e) = 0.591 \text{ W}/(\text{m} \cdot \text{K})$

$Q = 11.813 \text{ W}/\text{m}$

$t_i = 20.00^\circ\text{C}$

$t_e = 0.00^\circ\text{C}$

$U_{p1} = 5.033 \text{ W}/(\text{m}^2 \cdot \text{K})$ (right edge of bitmap)

$w_{p1} = 0.1900 \text{ m}$ (distance no. 2)

$U_{p2} = 0.000 \text{ W}/(\text{m}^2 \cdot \text{K})$

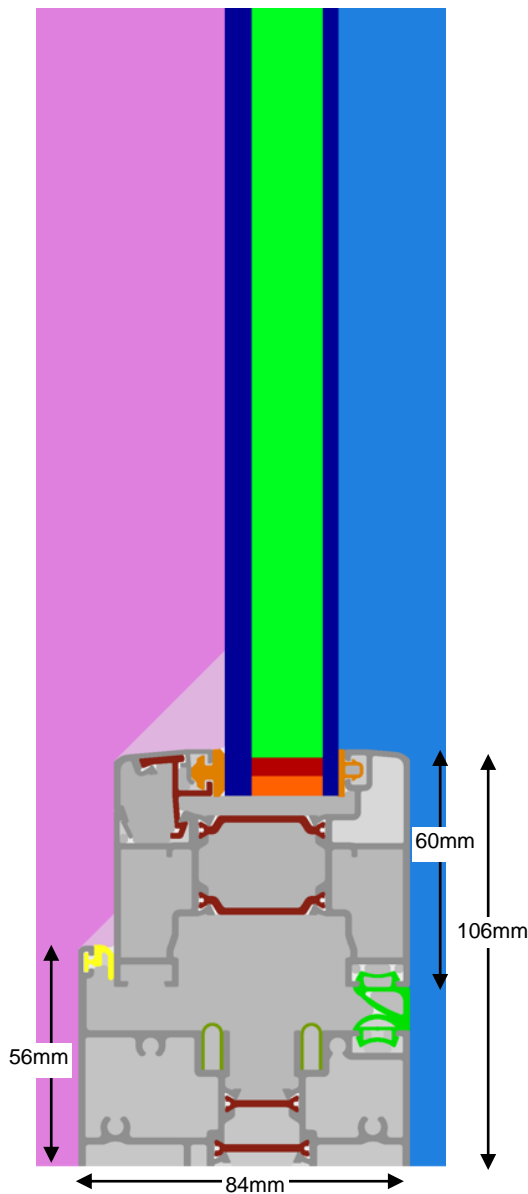
$w_{p2} = 0.0000 \text{ m}$

$w_f = 0.1059 \text{ m}$ (distance no. 1)

	Material	Thermal Conductivity W/(m.K)
	PVC-U Rigid, BS EN 10077-2	0.17
	PVC Flexible, BS EN 10077-2	0.14
	Aluminium, BS EN 10077-2	160.0
	Soda Lime Glass, BS EN 10077-2	1.0
	Superspacer Premium, IFT Rosenheim report 13-002649-PR02 (declared value)	0.15
	Hot Melt Butyl, BS EN 10077-2	0.24
	Polyurethane Foam, BS 10456	0.05
	EPDM, BS EN 10077-2	0.25
	Polyamide, BS EN 10077-2	0.30

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Threshold



BISCO Calculation Results

BISCO data file: A-04114 threshold.bsc

Number of nodes = 68998
 Heat flow divergence for total object = 0.000865678
 Heat flow divergence for worst node = 0.354333

Thermal transmittance of frame (EN 10077-2)
 $U_f = (Q / (t_i - t_e) - U_{p1} * w_{p1} - U_{p2} * w_{p2}) / w_f = -3.430 \text{ W}/(\text{m}^2 \cdot \text{K})$
 Thermal coupling coefficient

$L2D = Q / (t_i - t_e) = 0.593 \text{ W}/(\text{m} \cdot \text{K})$

$Q = 11.870 \text{ W}/\text{m}$

$t_i = 20.00^\circ\text{C}$

$t_e = 0.00^\circ\text{C}$

$U_{p1} = 5.033 \text{ W}/(\text{m}^2 \cdot \text{K})$ (top edge of bitmap)

$w_{p1} = 0.1900 \text{ m}$ (distance no. 2)

$U_{p2} = 0.000 \text{ W}/(\text{m}^2 \cdot \text{K})$

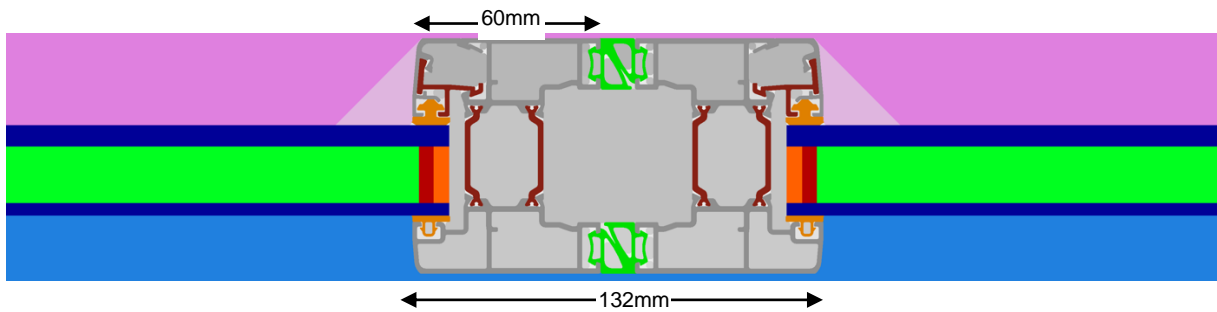
$w_{p2} = 0.0000 \text{ m}$

$w_f = 0.1058 \text{ m}$ (distance no. 1)

	Material	Thermal Conductivity W/(m.K)
	PVC-U Rigid, BS EN 10077-2	0.17
	PVC Flexible, BS EN 10077-2	0.14
	Aluminium, BS EN 10077-2	160.0
	Soda Lime Glass, BS EN 10077-2	1.0
	Superspacer Premium, IFT Rosenheim report 13-002649-PR02 (declared value)	0.15
	Hot Melt Butyl, BS EN 10077-2	0.24
	Polyurethane Foam, BS 10456	0.05
	EPDM, BS EN 10077-2	0.25
	Polyamide, BS EN 10077-2	0.30

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Meeting Stile



BISCO Calculation Results

BISCO data file: A-04117 meeting stile.bsc

Number of nodes = 101901

Heat flow divergence for total object = 0.00037338

Heat flow divergence for worst node = 0.696044

Thermal transmittance of frame (EN 10077-2)

$U_f = (Q / (t_i - t_e) - U_{p1} * w_{p1} - U_{p2} * w_{p2}) / w_f = -7.796 \text{ W/(m}^2 \cdot \text{K)}$

Thermal coupling coefficient

$L2D = Q / (t_i - t_e) = 0.886 \text{ W/(m} \cdot \text{K)}$

$Q = 17.719 \text{ W/m}$

$t_i = 20.00^\circ\text{C}$

$t_e = 0.00^\circ\text{C}$

$U_{p1} = 5.033 \text{ W/(m}^2 \cdot \text{K)}$ (left edge of bitmap)

$w_{p1} = 0.1900 \text{ m}$ (distance no. 2)

$U_{p2} = 5.033 \text{ W/(m}^2 \cdot \text{K)}$ (right edge of bitmap)

$w_{p2} = 0.1900 \text{ m}$ (distance no. 3)

$w_f = 0.1317 \text{ m}$ (distance no. 1)

	Material	Thermal Conductivity W/(m.K)
	PVC-U Rigid, BS EN 10077-2	0.17
	PVC Flexible, BS EN 10077-2	0.14
	Aluminium, BS EN 10077-2	160.0
	Soda Lime Glass, BS EN 10077-2	1.0
	Superspacer Premium, IFT Rosenheim report 13-002649-PR02 (declared value)	0.15
	Hot Melt Butyl, BS EN 10077-2	0.24
	Polyurethane Foam, BS 10456	0.05
	EPDM, BS EN 10077-2	0.25
	Polyamide, BS EN 10077-2	0.30

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